

REAL-WORLD SORTING OF RHIC SUPERCONDUCTING MAGNETS*

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Abstract

During the seven-year construction of the Relativistic Heavy Ion Collider (RHIC), more than 1700 superconducting dipoles, quadrupoles, sextupoles, and multi-layer correctors have been constructed and installed. These magnets have been sorted at several production stages to optimize their performance and reliability. For arc magnets, priorities have been put first on quench performance and operational risk minimization, second on field transfer function and other first-order quantities, and finally on nonlinear field errors which were painstakingly optimized at design. For Interaction-Region (IR) magnets, sorting is applied to select the best possible combination of magnets for the low- β^* interaction points (IP). This paper summarizes the history of this real-world sorting process.

1 INTRODUCTION

The RHIC magnet system consists primarily of superconducting dipole, quadrupole, sextupole and corrector magnets for guiding, focusing, and correcting the counter-circulating ion beams into the design orbits in the regular arcs of the machine lattice. A large complement of special superconducting magnets is also required for steering the beams into collisions at the six interaction regions (IR) where the ion beams interact. During the seven-year construction cycle, more than 1700 superconducting magnets have been constructed, measured, installed and tested. In order to optimize the performance of these magnets, sorting has been applied whenever possible.

For a majority of the arc magnets, priorities have been put first on quench performance and operational risk minimization and second on field transfer function and other first-order quantities. Since nonlinear field errors were painstakingly optimized at design, and their sorting priority was low. For IR magnets, sorting was applied to select the best possible combination of magnets for 2 out of 6 IRs where β^* will be lowered to 1 meter for high luminosity experiments. In order to minimize the relative misalignment between magnets in a common cryostat, sorting was also applied both before and after cryostat assembly. In contrast to an idealized magnet sorting, sorting in a real world is often constrained by the assembly and installation schedule, available storage space, etc. This paper summarizes the history of this real-world sorting process. In Section 2, we review the overall procedure of magnet analysis, acceptance, and sorting. In Sections 3 and 4, we summarize the actual sorting experience for arc and IR magnets.

2 MEASUREMENT DATA ANALYSIS

Besides reaching fields with substantial margins above the required range, all of the RHIC magnets must meet stringent requirements for field quality, reproducibility, and long-term reliability. In order to fulfill this goal, a committee of magnet division and RHIC accelerator physics personnel jointly reviewed the field quality, quench test performance, survey and other engineering aspects of the magnets. After individual magnet elements (coldmasses) are measured and tested, the magnetic field quality data, including transfer function, field angle, multipole harmonics, magnetic center offsets, etc. at all the test currents, [1] are recorded along with the warm mechanical survey measurements of the fiducial positions, sagitta, mechanical length and field angle. The data are transferred from the magnet division into the RHIC SYBASE database, and then analyzed by studying trends, comparing with the expected values, and evaluating the deviation from the mean using the computer program MAGSTAT [2]. As shown in Fig. 1, after their review and acceptance, magnets contained in their own cryostats (e.g. arc dipoles) are sorted for their candidate installation locations. Magnets belonging to a common cryostat assembly go through a second stage of

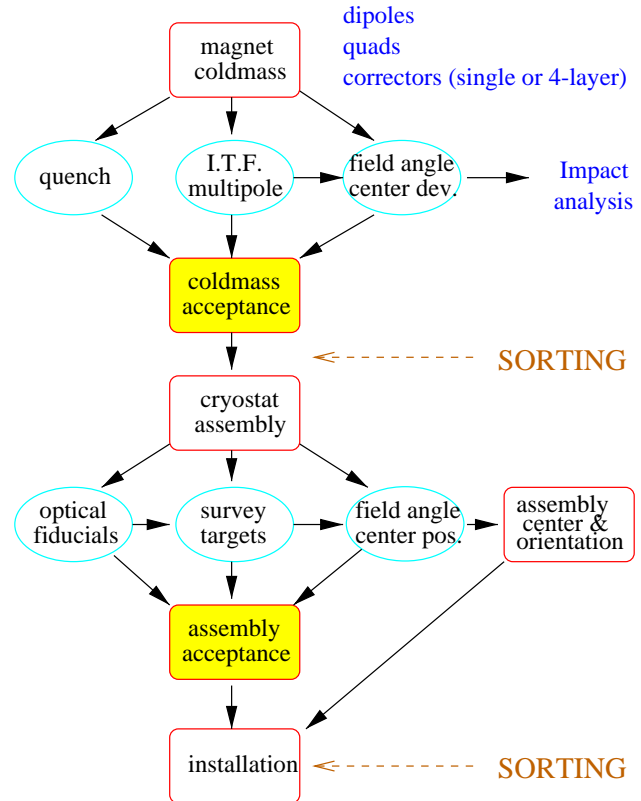


Figure 1: Magnet acceptance and sorting procedure.

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review, acceptance and sorting. At this stage, the assembly is surveyed with either colloidal-cell optical or stationary-coil pick-up (antenna) techniques to locate the magnetic centers of the components relative to the cold mass fiducials and the externally accessible cryostat fiducials. This survey data is transferred into the database and analyzed using the computer program SURVSTAT [3]. Based on a second-round review and balance of both coldmass and assembly data, the assemblies are sorted for final installation.

3 ARC REGION MAGNET SORTING

RHIC arc dipoles, quadrupoles and sextupoles are industry-built magnets. Despite close communication and detailed quality assurance procedures, unexpected changes in the manufacturing process still occurred. Magnet acceptance review and the subsequent sorting played an essential role in optimizing the final performance.

3.1 Arc Dipoles

During the acceptance, a drop in the integral transfer function (ITF) of about 0.1% was noticed and traced to the narrower width of the phenolic insulator used between the coil and the iron. Although the problem was corrected, about 20 magnets were affected. These magnets were sorted along with all subsequent dipole magnets. The sorting procedure was based on the strength minimization of dipole correctors required to compensate for the variation in the integral transfer function. With sorting, the maximum current required for such compensation was decreased from 12 A to about 3 A.

The dominant multipoles of the dipole magnets are b_2 (normal sextupole) and b_4 (normal decapole) resulting from the dipole symmetry of the magnets, and a_1 (skew quadrupole) resulting from the asymmetric vertical placement of the magnet cold mass in the cryostat. Due to the relatively high injection energy and the small diameter of the coil filaments, the persistent current effects are small. Magnet design has minimized b_2 and b_4 for both injection and storage currents by optimizing the cross-sections of the coil and the yoke taking into account the persistent current and saturation effects. The minimization of a_1 is achieved by sorting the yoke weight during the assembly process so that the lower half yoke is heavier than the upper half.

Among the eight dipoles allocated as spare magnets, five of them have off-normal skew quadrupole component (a_1 up to -5.9 units [4]), some caused by a known coil size mismatch; one has an excessive twist (2.5 mr standard deviation in body field angle) along the magnet body, and one has low transfer function at high fields.

3.2 Arc Quadrupoles

At the early stage of industrial manufacture, midplane shims were incorrectly changed on 5 quadrupoles, resulting in a b_3 of about -6 units. These magnets were sorted and distributed among the two rings to minimize their effects.

The dominant multipoles of the quadrupoles are b_5 and a_5 resulting from the quadrupole symmetry of the coil and

the end configuration, and b_3 resulting from the asymmetry between the horizontal and vertical planes. b_3 was compensated in the design by making the coil to midplane gap appropriately asymmetric, while b_5 was reduced by compensating the body with the ends of the magnet.

Among the eight quadrupoles allocated as spare magnets, four of them are of concern with off-normal coil size or low collaring pressure, some resulting in large a_2 ; two have excessive b_2 (-5 units); one has an engineering repair.

3.3 Arc Sextupoles

In general, the performance of the sextupole magnets exceeded the design goal. However, the epoxy contained in about 42 magnet coils is significantly weaker than normal. Consequently, the average quench currents (about 170 A) of these magnets, although exceeding the design operating current (100 A), are lower than the average of the regular magnets (above 200 A). To minimize possible long-term effects, these magnets have been sorted and allocated to the focusing locations around the two rings where the required strength of the sextupoles for chromaticity correction is about 50% of that at the defocusing locations.

3.4 Arc Trim Quadrupoles

Trim quadrupoles all have minimum quench currents above 200 A, well exceeding the design operating current of 100 A. One trim quadrupole coldmass was designated as a spare due to rust on the yoke caused by rain damage.

3.5 Arc Correctors

All of the correctors, either single-layer or four-layer, were built in-house and cold tested. After initial training, all the magnets quench above the design operating current of 50 A. Since the dipole corrector layers are all powered individually, the variation in the integral transfer function (typically 1% rms) is of little concern. Correctors with layers of excessive field angle deviation (up to ~ 20 mr) or erratic quench training were selected as spare magnets.

3.6 Arc CQS Assembly

Arc corrector, quadrupole, and sextupole magnets were welded into a single "CQS" assembly. The CQS assembly also includes a beam position monitor and (for some) a recoler. The CQS components need to be aligned with each other so that their magnetic centers are on a straight line. It was found in the early stage of installation that "Springs" (made of G-10 plastic) needed to be installed or refitted in the support posts, confining the coldmass transversely while allowing free longitudinal motion. Special welding stripes were applied to the CQS shell to align the magnetic centers of the individual coldmasses for assemblies that exceeded a tolerance of 0.25 mm. Subsequently, the welding sequence is carefully choreographed to balance "curling" distortions against each other.

Correctors with large misalignments can generate serious feed-down harmonics. Two early CQSs with corrector offsets larger than 2 mm have been removed from the tunnel, and were later corrected.

4 IR MAGNET SORTING

The IR triplet cryostat contains two dipoles, six quadrupoles, and six four-layer corrector packages of the two rings. Field imperfection of the IR magnets limits the machine performance at collision when β^* is squeezed. Among the 6 interaction points, 2 of them are planned to run at a low β^* of 1 m. Most sorting efforts have been to select the best IR magnets for these 2 “golden” IPs.

4.1 IR Dipoles

In general, two IR dipoles, one on each side of the IP, are powered by the same shunt power supply. Sorting has been performed to pair dipoles of similar transfer function to the same IP. Two dipoles with off-normal transfer function are assigned to special locations where individual shunt supplies exist. Early magnets with imperfect field quality (large b_2) were assigned to non-golden region. Since the outstanding random error is a_1 , magnets of similar a_1 are sorted to the opposite side of the same IP to minimize their action kicks [5]. One dipole is designated as a spare due to erratic quench performance.

4.2 IR Quadrupoles

The manufacturing sequence of IR quadrupoles follows the level of required performance, starting with the less-critical Q1. Several iterations were made on the magnet cross section to optimize the field quality. Application of tuning shims is also practiced at this stage.

In one Q2 quadrupole, an excessive amount of axial variation in multipole errors was found (change of 15 units of a_2) and suspected to be due to cracked insulators. The quench performance, though adequate, was lower than average. Efforts were made at the last stage of installation to replace this “golden candidate” with a “spare candidate”.

Due to lack of time for cryogenic testing, 11 out of 72 IR quadrupoles were measured only at room temperature. Because of imperfect correlation between the warm and cold measurements, the field quality of these magnets is less well known than the field quality of magnets which have been cold tested. Since this information is the critical base for IR correction, these magnets were sorted to “non-golden” IRs. Spare magnets were mostly selected based on off-normal multipole errors. One quadrupole with a partially inserted shim was first allocated as a spare but later installed to meet schedule requirements for the first sextant test.

4.3 IR Correctors

Sorting on IR correctors was performed along with the quadrupoles before their attachment to minimize the relative magnetic center offset and field angle. After sorting, for CQ combinations with excessive relative offset and roll, shimming adjustment were made before welding of the assembly.

4.4 IR CQ Assembly

IR correctors were welded to IR quadrupoles to form CQ assemblies. At a later stage of IR CQ assembly, electric

Table 1: Summary of RHIC magnet sorting ($n = 1$ is quadrupole).

Magnet	Number (used+spare)	Sorted quantity
Arc dipole	288+8	ITF, yoke weight (a_1) twist, b_2
Arc quad.	372+8	coil size, midplane shim size collaring pressure coil saddle crack repair, b_2
Arc sext.	288+12	epoxy level (quench)
Arc corr.	420+10	quench, field angle
D5I	12+1	vacuum vessel straightness
D5O	12+1	vacuum vessel straightness
D96	48+1	
Trim quad.	72+6	rust on yoke
CQS	282+8	corrector offset
CQT	72+6	
CQ	60+2	
Interaction region magnets:		
IR dipole	24+2	quench, ITF, b_2 , a_1
IR quad.	72+6	data availability (schedule) axial variation of a_2 partial shim, multipoles center offset, roll
IR corr.	72+6	
DX dipole	12+1	
IR CQ	72+6	potential corrector shorts
Total	1692+65	

shorts were found at the octupole leads of IR correctors precipitated by a routing misdesign. Rework was done on all the correctors which were still in coldmass state. For correctors designated as “golden” and yet with their end plates already welded on, their end plates were removed to allow a complete rework. About 8% of the CQ assemblies fully installed in the machine were not reworked, and their chance of octupole layer malfunction is less than 10%.

4.5 Separating Dipoles DX

After a design iteration based on the prototype magnet, the field errors (b_2 , b_4) of these large-bore (18 cm coil diameter) dipoles were greatly reduced and are well within the capability of IR correction [6].

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